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FORMULATION OF BALANCE OF FORCES IN MIXTURE THEORIES*

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1. Introduction. The fundamental concept of the continuum theory of mixtures, that of modeling the mixture as a collection of distinct continuous bodies coexistent in space, is both clear and intuitively pleasing. However, it is not a simple matter to decide what form the corresponding equations of balance should take. In [1] Oliver introduced an axiomatic derivation of balance laws for mixtures of rigid continua; in [2] Williams extended the axioms to motions of non-diffusive mixtures. It was hoped that such derivations might serve to give a more substantial base to the classical field theories for mixtures, but in fact the resulting equations differ significantly from the usual ones.

In this paper we illustrate these distinctions by considering the equation of balance of forces for a non-diffusive mixture. We present the classical formulation, then the formulation of Oliver and Williams and finally a related but different formulation which has been suggested in a note by Gurtin, Oliver and Williams [3].

2. Geometry, definitions. Let \mathcal{E} denote three-dimensional euclidean space, and B denote a smooth regular open region in \mathcal{E} . We call B the *body*. Let \mathbf{B} denote the collection of all smooth regular open regions contained in B . Each element A in \mathbf{B} is called a *subbody* of B .

We define operations \vee and \wedge on $\mathbf{B}^2 = \mathbf{B} \times \mathbf{B}$ and $*$ on \mathbf{B} as follows:

$$A \vee C = A \cup C, \quad A \wedge C = \overline{A \cap C}, \quad A^* = \overline{B/A}.$$

We say that elements $A, C \in \mathbf{B}$ are *separate* if $A \wedge C = \emptyset$, and we let $\text{sep } \mathbf{B}^2$ denote the collection of separate pairs (A, C) in \mathbf{B}^2 .

By a *mixture* we mean a body B together with its collection \mathbf{B} of subbodies and an index set $I = \{1, 2, \dots, n\}$ whose elements are called *constituents*. Physically, of course, we picture the mixture as a set of spatially coincident bodies within the region B . For each constituent i in I and element A in \mathbf{B} , A_i shall denote the part of constituent i occupying the region A in B . We shall refer to B_i as the i th constituent body.

Let \mathcal{V} designate the translation space of \mathcal{E} . We define a *force system* for a non-diffusive mixture to be a collection of functions $F_{ii}, F_i^e, i, j \in I$ with the following properties:

$$\begin{aligned} F_{ii}: \mathbf{B}^2 \rightarrow \mathcal{V}, & \quad i \neq j \\ F_{ii}: \text{sep } \mathbf{B}^2 \rightarrow \mathcal{V}, & \quad F_i^e: \mathbf{B} \rightarrow \mathcal{V}; \end{aligned} \tag{i}$$

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$$F_{i,i} \text{ is biadditive;}^1 \quad (\text{ii})$$

$$F_{i,i}^\circ \text{ is additive.}^1 \quad (\text{iii})$$

For $(A, C) \in \mathbf{B}^2$, $F_{i,i}(A, C)$ is the force exerted by C_i on A_i ; for $A \in \mathbf{B}$, $F_{i,i}^\circ(A)$ is the force exerted on A , by the environment of B (including inertial forces).

Given a force system for a mixture, we define for each $i \in I$ a new function $F_{i,i}: \mathbf{B}^2 \rightarrow \mathcal{U}$ as follows:

$$F_{i,i}(A, C) = \sum_{\substack{j \in I \\ j \neq i}} F_{i,j}(A, C) + F_{i,i}(A, \overline{C - A}) + F_{i,i}(\overline{A - C}, A \wedge C). \quad (1)$$

Note that (1) is defined even when $A \wedge C \neq \emptyset$. For $(A, C) \in \mathbf{B}^2$, we call $F_{i,i}(A, C)$ the force exerted on A_i by the mixture within C .

If forces are prescribed on parts of ∂B , we suppose that they are prescribed for each constituent; that is, if $\mathcal{S} \subset \partial B$.

$$f_i: \mathcal{S} \rightarrow \mathcal{U}$$

is given as the force on \mathcal{S} which must be supported by the i th constituent.

3. Balance of forces in classical mixture theory. In classical mixture theory the law of *balance of forces* takes the form

$$F_{i,i}(A, B) + F_{i,i}^\circ(A) = 0 \quad \text{for all } i \in I, A \in \mathbf{B}. \quad (2)$$

This requires that the force exerted on A_i by the mixture plus the force exerted on A_i by the environment of B must be zero. The forces in (2) and (1) are presumed to be represented as follows:

$$F_{i,i}(A, C) = \int_{\partial A \cap \partial C} T_i n \, da, \quad (3)$$

for every $(A, C) \in \text{sep } \mathbf{B}^2$, where n is the unit normal to ∂A ;

$$F_{i,i}(A, C) = \int_A p_i \, dv + \int_{\partial A \cap C} T_i n \, da \quad (4)$$

for every $(A, C) \in \mathbf{B}^2$ with $A \subseteq C$;

$$F_{i,i}^\circ(A) = \int_A b_i^\circ \, dv + \int_{\partial A \cap \partial B} T_i n \, da, \quad (5)$$

for every $A \in \mathbf{B}$. Here T_i , b_i° and p_i are respectively $\mathcal{L}(\mathcal{U})$, \mathcal{U} , \mathcal{U} -valued functions on B with the following interpretations: T_i is the *partial stress tensor* for constituent i , b_i° the *external body force* on constituent i , and p_i the total *diffusive force* exerted on constituent i . Using (3)–(5), we can write (2) in the following integral form:

$$\int_{\partial A \cap B} T_i n \, da + \int_A p_i \, dv + \int_A b_i^\circ \, dv + \int_{\partial A \cap \partial B} T_i n \, da = 0,$$

¹ A function $F: \mathbf{B} \rightarrow \mathcal{U}$ is *additive* if $F(A \vee C) = F(A) + F(C)$ whenever A, C , and $A \vee C$ all belong to \mathbf{B} and $(A, C) \in \text{sep } \mathbf{B}^2$. A function $F: \mathbf{B} \rightarrow \mathcal{U}$ is *biadditive* if it is additive in each argument, i.e., if $F(A \vee C, D) = F(A, D) + F(C, D)$ and $F(A, D \vee E) = F(A, D) + F(A, E)$ whenever $A, C, D, E, A \vee C$ and $D \vee E$ all belong to \mathbf{B} and $(A, C), (D, E) \in \text{sep } \mathbf{B}^2$.

for every $A \in \mathbf{B}$. Locally this last equation reduces to

$$\operatorname{div} T_i + p_i + b_i^* = 0 \quad \text{for all } i \in I. \quad (6)$$

Defining² $T = \sum_{i \in I} T_i$ as the *global stress tensor* and using (6), we obtain

$$\operatorname{div} T + \sum_{i \in I} (p_i + b_i^*) = 0. \quad (7)$$

In order to guarantee balance of forces *for the mixture as a whole*, the classical theory requires that

$$\int_{\partial A} T n \, da + \int_A (\sum_{i \in I} b_i^*) \, dv = 0$$

for every $A \in \mathbf{B}$; locally this reduces to

$$\operatorname{div} T + \sum_{i \in I} b_i^* = 0. \quad (8)$$

Eqs. (7) and (8) require

$$\sum_{i \in I} p_i = 0. \quad (9)$$

If forces f_i be prescribed on $s \subset \partial B$, then the boundary conditions for T_i are

$$T_i n|_s = f_i. \quad (10)$$

Eqs. (6) and (9), together with the boundary conditions (10), are the equations of force balance for the classical theory.

4. Balance of forces in the OW theory. The axiomatic approaches to the theory of mixtures proposed by Oliver [1] and Williams [2] impose more stringent requirements on the system. Balance of forces for A_i alone is ensured by (2) as in the classical theory. But, in addition, the requirement of balance of forces for such compound elements as $A_i \cup A_j$ leads to the following set of balance equations:

$$F_{i,j}(A, B) + F_i^*(A) = 0 \quad (2)$$

for all $i \in I$, $A \in \mathbf{B}$, and

$$F_{i,j}(A, C) + F_{i,i}(C, A) = 0 \quad (11)$$

for all $i, j \in I$, $i \neq j$, all $(A, C) \in \mathbf{B}^2$. Eq. (11) is also required to hold for $i = j$ provided that $(A, C) \in \operatorname{sep} \mathbf{B}^2$. Moreover, the axiomatic scheme yields the following representations:

$$F_{i,j}(A, C) = \int_{\partial A \cap \partial C} \sigma_{ij}^{\partial A} \, da \quad (12)$$

for every $(A, C) \in \operatorname{sep} \mathbf{B}^2$ and all $i, j \in I$;

$$F_{i,i}(A, C) = \int_A p_{ii} \, dv + \int_{\partial A \cap \partial C} \tau_{ii}^{\partial A} \, da, \quad (13)$$

² For simplicity, we assume that the diffusive velocities are zero; the equation of balance for the mixture as a whole is much more complicated in the general case.

for every $(A, C) \in \mathbf{B}^2$ with $A \subseteq C$ and for all $i, j \in I$ with $i \neq j$;

$$F_i^e(A) = \int_A b_i^e dv + \int_{\partial A \cap \partial B} f_i da \quad (14)$$

for every $A \in \mathbf{B}$ and $i \in I$. Here σ_{ij}^s and τ_{ij}^s are defined for any smooth manifold s in B and map s into \mathcal{U} ; f_i maps ∂B into \mathcal{U} ; p_{ij} and b_i^e map B into \mathcal{U} . Here $\sigma_{ij}^{\partial A}$ is the density of the force exerted on A_i by C_j through the surface of contact $\partial A \cap \partial C$; $\tau_{ij}^{\partial A}$ is the density of the force exerted on A_i by A_j through the surface ∂A ; f_i is the density of the force exerted on B_i by the environment of B across the surface of contact ∂B ; p_{ij} is the density of the diffusive force exerted by B_j on B_i , and b_i^e is as before.

In addition the axiomatic scheme yields for all $i, j \in I$

$$\tau_{ij}^s = -\sigma_{ij}^s \quad (i \neq j), \quad (15)$$

for every smooth manifold s in \mathring{B} . By using Eqs. (12)–(15) the balance Eq. (2) becomes

$$\int_{\partial A} \sigma_{ii}^{\partial A} da + \int_A (p_i + b_i^e) dv = 0, \quad (16)$$

for every $A \in \mathbf{B}$ with $\partial A \cap \partial B$ of zero area and for every $i \in I$; here we have set $p_i = \sum_{j \in I, j \neq i} p_{ij}$. The balance equation (11) becomes

$$-\int_{\partial A} (\sigma_{ij}^{\partial A} + \sigma_{ji}^{\partial A}) da + \int_A (p_{ij} + p_{ji}) dv = 0, \quad (17)$$

for every $A \in \mathbf{B}$ and all $i, j \in I$ with $i \neq j$; and

$$\int_s (\sigma_{ij}^s + \sigma_{ji}^{-s}) da = 0, \quad (18)$$

for every $s \subset \mathring{B}$ and all $i, j \in I$. It follows from (15)–(18) that there exist mappings T_{ij} from B into $\mathcal{L}(\mathcal{U})$ such that

$$\begin{aligned} \sigma_{ii}^s &= T_{ii}n, \\ \sigma_{ij}^s + \sigma_{ji}^s &= T_{ij}n \quad (i \neq j), \end{aligned}$$

for every smooth manifold s in B , where n is the positive unit normal to s . T_{ij} is the ij stress tensor. The local forms of (16), (17), and (18) are

$$\begin{aligned} \operatorname{div} T_{ii} + p_i + b_i^e &= 0, \\ \operatorname{div} T_{ij} - p_{ij} - p_{ji} &= 0, \quad i \neq j, \\ \sigma_{ij}^s + \sigma_{ji}^{-s} &= 0, \quad i \neq j. \end{aligned} \quad (19)$$

The complete set of local balance equations is then given by (19). If forces f_i be prescribed on $s \subset \partial B$ for the i th constituent, then boundary conditions for this system are

$$T_{ii}n|_s - \sum_{\substack{j \in I \\ j \neq i}} \tau_{ij}^s = f_i, \quad (20)$$

$$T_{ij}n|_s + \tau_{ij}^s + \tau_{ji}^s = 0.$$

The latter can also be written, using (15), as

$$T_{ij}n|_s - \sigma_{ij}^s - \sigma_{ji}^s = 0.$$

By construction there are no further conditions necessary in order to guarantee balance of forces for the entire mixture.

If we define $T_i = \sum_{j \in I} T_{ij}$ and $\hat{p}_i = - \sum_{j \in I, j \neq i} p_{ji}$, summing (19)₂ over $j \neq i$ and adding the result to (19)₁ yields

$$\operatorname{div} T_i + \hat{p}_i + b_i^\epsilon = 0, \tag{21}$$

which is exactly of the form (6). However, the boundary conditions for T_i are, using (20),

$$T_i n|_s + \sum_{\substack{j \in I \\ j \neq i}} \tau_{ij}^s = f_i, \tag{22}$$

which differs from (10). Recapitulating, for this system, the basic equations are (19) with boundary conditions (20); as a consequence of these we obtain the balance equation (21) with boundary condition (22) (of course (21), (22) do not suffice to guarantee (19), (20)). As a consequence of the above, we have for the *global stress tensor*, defined to be

$$T = \sum_{\substack{i, j \in I \\ i < j}} T_{ij},$$

the equation

$$\operatorname{div} T + \sum_{\substack{j \in I \\ j \neq i}} (p_i + b_i^\epsilon) = 0.$$

5. Balance of forces in the GOW theory. In (3) Gurtin, Oliver and Williams suggest representations differing from the previous ones. We again shall require balance of force for all combinations of constituent bodies and therefore introduce balance Eqs. (2) and (11). The representation formulae are

$$F_{ij}(A, C) = \int_{\partial A \cap \partial C} \sigma_{ij}^{\partial A} da \tag{23}$$

for every $(A, C) \in \operatorname{sep} \mathbf{B}^2$ and all $i, j \in I$;

$$F_{ij}(A, C) = \int_A p_{ij} dv + \int_{\partial A} \tau_{ij}^{\partial A} da + \int_{\partial A \cap C} \sigma_{ij}^{\partial A} da \tag{24}$$

for every $(A, C) \in \mathbf{B}^2$ with $A \subseteq C$ and all $i, j \in I$ with $i \neq j$;

$$F_i^\epsilon(A) = \int_A b_i^\epsilon dv + \int_{\partial A \cap \partial B} f_i da \tag{25}$$

for every $A \in \mathbf{B}$ and $i \in I$. The density functions σ_{ij}^s and τ_{ij}^s are defined on any smooth manifold \mathcal{S} in B and map \mathcal{S} into \mathcal{V} ; f_i maps ∂B into \mathcal{V} ; p_{ij} and b_i^ϵ are as before. The interpretations of σ_{ij}^s and τ_{ij}^s are the same as before.³ The balance equations (2) and (11) become in this scheme:

$$\int_{\partial A} (\sigma_{iI}^{\partial A} + \tau_{iI}^{\partial A}) da + \int_A (p_i + b_i^\epsilon) dv = 0 \tag{26}$$

³ The distinction between this and the previous representations is made clear by examining $F_{ij}(A, C)$ where $\bar{A} \subset C$. OW requires $F_{ij}(A, C) = \int_A p_{ij} dv$, while GOW requires $F_{ij}(A, C) = \int_A p_{ij} dv + \int_{\partial A} (\sigma_{ij}^{\partial A} + \tau_{ij}^{\partial A}) da$. GOW reduces to OW if we require, as is a consequence of the axiom scheme of OW, that $\sigma_{ij}^s + \tau_{ij}^s = 0$ for all \mathcal{S} (cf. (15)).

for every $A \in \mathbf{B}$ and $i \in I$;

$$\int_{\partial A} (\tau_{ij}^{\partial A} + \tau_{ji}^{\partial A}) da + \int_A (p_{ii} + p_{ji}) dv = 0 \tag{27}$$

for every $A \in \mathbf{B}$ and all $i, j \in I$ with $i \neq j$;

$$\int_{\mathcal{S}} (\sigma_{ij}^{\mathcal{S}} + \sigma_{ji}^{-\mathcal{S}}) da = 0 \tag{28}$$

for every smooth manifold \mathcal{S} in B and all $i, j \in I$. Here

$$\sigma_{iI}^{\mathcal{S}} = \sum_{j \in I} \sigma_{ij}^{\mathcal{S}}, \quad \tau_{iI}^{\mathcal{S}} = \sum_{\substack{j \in I \\ j \neq i}} \tau_{ij}^{\mathcal{S}},$$

and p_i is as before.

In order to ensure that the force functions are additive it is necessary that

$$\sigma_{ij}^{\mathcal{S}} + \tau_{ij}^{\mathcal{S}} = -\sigma_{ji}^{-\mathcal{S}} - \tau_{ji}^{-\mathcal{S}} \quad (i \neq j), \tag{29}$$

for all \mathcal{S} . From (26), (27) and (29) we may deduce the existence of *stress tensor fields* $T_{ij}: B \rightarrow \mathcal{L}(\mathcal{V})$ such that

$$\sigma_{iI}^{\mathcal{S}} + \tau_{iI}^{\mathcal{S}} = T_{iI}n \tag{30}$$

and

$$\tau_{iI}^{\mathcal{S}} + \tau_{ji}^{\mathcal{S}} = -T_{ij}n,$$

where n is the unit normal to the smooth surface \mathcal{S} . (The choice of the minus sign in (30)₂ is to make the equations parallel those of Sec. 4.) The local forms of (26), (27) and (28) are now

$$\begin{aligned} \operatorname{div} T_{ii} + p_i + b_i^e &= 0, \quad \text{all } i, \\ \operatorname{div} T_{ij} - p_{ij} - p_{ji} &= 0, \quad i \neq j, \\ \sigma_{ij}^{\mathcal{S}} + \sigma_{ji}^{-\mathcal{S}} &= 0. \end{aligned} \tag{31}$$

Eqs. (31) comprise the complete set of local balance equations if (29) is also required. Eqs. (31) are formally the same as (19), and indeed would reduce to (19) if it were required that $\sigma_{ij}^{\mathcal{S}} = -\tau_{ij}^{\mathcal{S}}$ for all \mathcal{S} . Given boundary forces f_i on $\mathcal{S} \subset \partial B$, the *boundary equations* for this system are

$$\begin{aligned} T_{iI}n |_{\mathcal{S}} - \sum_{\substack{j \in I \\ j \neq i}} \tau_{ij}^{\mathcal{S}} &= f_i, \\ T_{ij}n |_{\mathcal{S}} + \tau_{ij}^{\mathcal{S}} + \tau_{ji}^{\mathcal{S}} &= 0. \end{aligned} \tag{32}$$

Again (32) is exactly the same as (20). Thus, except for the auxiliary condition (29), this formulation yields *exactly the same local equations of balance, with the same boundary conditions* as the formulation in Sec. 4.

As before, there are no further equations necessary to guarantee the balance of forces, but exactly as before it is possible to formulate a global stress balance equation for the entire mixture and to introduce the stress tensors T_i which apparently correspond to the classical stress tensors.

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